



REDUCTION OF GROUND VIBRATION BY MEANS OF GROUND IMPROVEMENT ALONG A RAILWAY TRACK

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Abstract

The ground vibrations induced by high-speed train have drawn engineering attention in recent years, since high-speed trains are growing rapidly throughout Europe, East Asia, and North America. Deep mixing technology, that has a wide range of application in the construction industry, has been used to mitigate the detrimental effects of vibration caused by high-speed trains. Deep mixing is a ground modification technology that mixes in situ soil with a cementitious material to produce overlapped columns using specially designed equipment with paddles and/or augers. This paper aims to examine and synthesize the latest advancements when deep mixing technology is used as the countermeasure against vibration control. Excitation mechanism caused by a moving load that provides the basis for train induced vibration is discussed. The current state of practice to analyse and predict the response of treated ground based on the analytical and numerical solutions are presented along with a summary of field data. The rigorous numerical solutions with 3-D modelling capabilities have demonstrated effective tools to predict improvement effect of deep mixing as a countermeasure for vibration control.

1. INTRODUCTION

Increased demand for higher speed to shorten travel time creates disturbance to human and the environment due to strong vibration. Therefore, vibration reduction has become a topic of special interest in recent years as the speed of train systems is mounting. Experience shows that the vibration induced by the high-speed rail can reach levels that cause human annoyance, possible damage to old and historical buildings, and interruption of sensitive instrumentation and processes [1]. In addition, there are rising concerns over the running safety of the trains, degradation of the embankment and foundation soil, fatigue failure of the rails, and disruption of power supply to the trains. To resolve the vibration problems, various mitigation strategies have been proposed. Therefore, the selection of a suitable vibration mitigation strategy becomes a challenging issue for engineers.

Deep mixing technology, as discussed in the following sections, is an innovative technique that is being used to mitigate the detrimental effects of vibration caused by high-speed trains. The current state of practice to analyze and predict the response of treated ground based on analytical and numerical solutions are discussed along with a summary of rare field data from Japan. Next section deals with excitation mechanism caused by a moving load that provides the basis for train induced vibration.

2. EXCITATION MECHANISM

The need for straight railway line to support high-speed train may force a route to pass through soft and compressible soils, such as organic soils, peat, and soft marine clays. Actual observations and measurements with high-speed trains have revealed that one might observe remarkably large vibrations in soft soil sites from the moving-load excitation mechanism [2]. Sites with low shear-wave velocities, in the range of 30 to 40 m/s, are particularly susceptible to excessive vibration from high-speed trains. Many factors influence the ground vibration amplitude and spectrum induced by high-speed train. Basically, ground vibrations by railway traffic are generated by two prime excitation mechanisms (a) the quasi-static displacement caused by the axle load as the wheel moves along the track, and (b) the inertia forces due to the acceleration of the unsprung mass of the train as it rolls over the irregular profile of the railhead, as shown Figure 1 and 2.

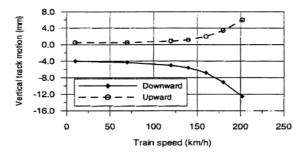


Figure 1. Average measured vertical displacement of track for different train speeds

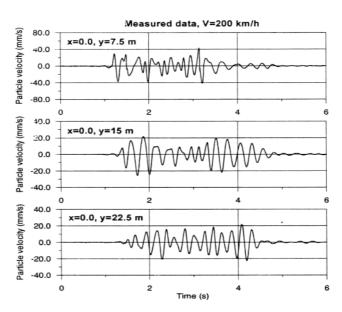


Figure 2. Measured track-side vibration for train speed 200km/h

At low speeds, the ground response from a moving load is essentially quasi-static. That is, the displacements and stress fields are essentially the static fields under the load simply moving with it. However, as the speed of the load increases, dynamic phenomena gradually take over and dominate the response. Figure 2 illustrates recordings at 7.5m, 15m, and 22.5m from the track for a train with a train speed of 200 km/h in Sweden [3,4].

3. DEEP MIXING TECHNOLOGY

Deep mixing is a ground modification technology (see Figure 3) that mixes in situ soil with a cementitious material (such as cement, lime, etc) using specially designed equipment with paddles and/or augers. The advantages of deep mixing are: (a) accelerated construction process (in terms of reducing construction time); (b) wide range of finished products (in terms of controllable strength, stiffness, etc) (c) environmentally friendliness (in terms of noise and vibration for construction in the urban areas), and (d) wide spectrum of applications in the construction industry. The scope of the application of deep mixing is to handle and solve problems associated with:

- Increasing bearing capacity
- Reduction of settlement
- Hydraulic barrier (controlling seepage and cutoff systems for containment)
- Seismic/liquefaction mitigation (reducing shear deformation)
- Remediation/immobilization/confinement of contaminated ground
- Increasing drivability for tunneling in soft ground; and
- Vibration impediment

Current methods for analysis of ground treated by deep mixing technology to impede vibration are discussed below.

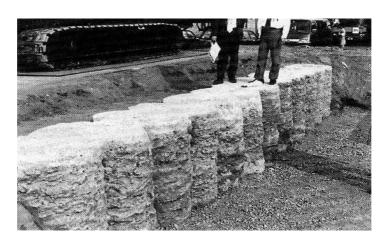


Figure 3. Deep mixing technology: treated ground in Japan

4. CURRENT METHODS OF ANALYSIS

Moving loads, such as high-speed trains, have long been recognized as potential source of ground vibration. The ground response to a moving load is dictated largely by the relation between the load speed and the characteristic wave velocities of the ground medium [1,4]. Analytical and numerical Methods have been proposed to predict the effect of ground response and vibration impediments when deep mixing is used as the countermeasure.

4.1 Analytical Approach

The vibration generated by a vibrating source (such as high speed trains, vibratory machines) is generally damped with distance. Distance damping is influenced mainly by ground condition and the wave properties at the surface, as follows:

$$\frac{u_x}{u_o} = \sqrt{\frac{x_0}{x}} \cdot \exp\{-\beta(x - x_0)\}\tag{1}$$

Where u_x : vibrational acceleration at x(m) from vibration source; u_0 : vibrational acceleration at $x_0(m)$ from vibration source and near the source; and β : damping coefficient. When deep mixing is used, the impedance effect of wave in the treated ground is taken into consideration. Generally, when a material with different stiffness/density exists inside the ground, the propagated wave from a source behaves such that a portion of the waves reflects due to impedance difference. And the rest is transmitted but reflects as it propagates outside the barrier that obstructs the vibration. The reduction ratio of wave (ratio between transmitting wave and incoming wave) is estimated using the wave propagation theory, as follows:

$$\tau_0 = 4\alpha / \{ (1 + \alpha)^4 + (1 - \alpha)^4 - 2(1 - \alpha^2)^2 \times \cos(4\pi f t / V') \}^{1/2}$$
(2)

Where: $\alpha = \rho' V'/\rho V$; ρ (Mg/m3): density of ground; ρ' (Mg/m3): density of blocking layer; V (m/sec): wave propagation speed of ground; V' (m/sec): wave propagation speed of blocking layer; t (m): blocking layer thickness; and f (Hz): frequency of the wave.

4.2 Numerical Approach

The ground was modeled as a layered visco-elastic half space, and the track embankment was modeled as a layered visco-elastic beam that interacts with the ground at discrete points. The model used the Kausel-Roesset Green's function to obtain the soil stiffness matrix at the ground-embankment interface nodes and assembled with the dynamic stiffness matrix of the embankment [7]. The solution was carried out in the frequency domain and the time histories of the motions were calculated through a Fourier synthesis of frequency components. Figure 4 shows typical results obtained for this study. The numerical solution was used to demonstrate the effectiveness of strengthening the embankment for mitigating ground vibration.

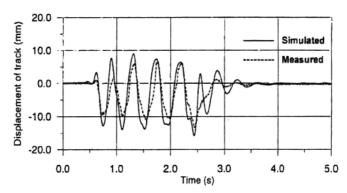


Figure 4. Time history of vertical track motion at a speed of V = 200 km/h

5. FIELD TESTS

Field tests have been performed in Japan to measure ground vibration and predict the effect of countermeasures by high-speed trains. The test site was in the Ariake Sea side of Rokkaku River, which is located in Southwest part of the Saga Plan in Western Japan [5]. Before the test undistracted samples from the site were collected with thin wall sampling method. Soil profile consists of 0.7m surface fill underlain by Ariake clay layer down to 13.5m resting on 1.5m sand layer. The unconfined compressive strength of clay starts from 20kPa at the top and increases with depth to reach 40kPa at the bottom of the clay layer. The moisture content was 100% to 120%. The treated ground consists of deep mixed continuous walls of 15m long, 7m deep, made of columns of 1.14m diameters with 20cm of outer overlapped edge. The binder is a cement-based solidification agent consisting of blast furnace cement and hydrated lime. Figure 5 shows the scheme of the field vibration test site. The purpose of the experiment was not for high-speed train, but to understand the vibration impedance caused by heavy construction machinery on deep mixed treated ground.

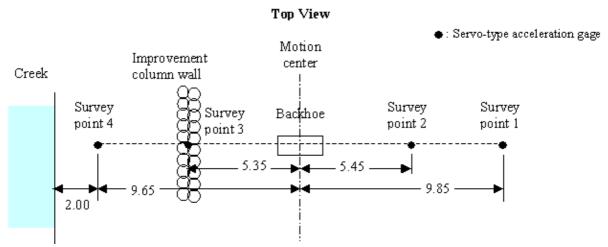


Figure 5. Layout of instrumentation for field vibration test in Japan

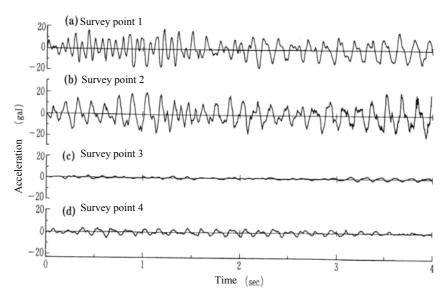
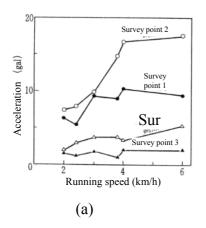


Figure 6. Measured Time history of Accelerations at Four Locations

Figure 6 shows the acceleration-time history for four surveyed points obtained from field tests at the speed of 4km/h of heavy machinery's running speed. Survey point 4 that has about the

same distance with survey point 1 from running position experienced drastic reduction in amplitude compared with that at survey point 1 due to the existence of treated columns. Figure 7a illustrates the relationship between running speed and generated acceleration. From this figure, the survey at point 3 with deep mixed columns has the lowest recorded acceleration. Figure 7b shows the damping of vibration acceleration with respect to distance. More specifically, at the location in which deep mixed columns are installed, (survey point 3) the generated acceleration is readily small. This is attributed to the stiffness of the treated ground that dampens vibration acceleration. Using the analytical solution discussed earlier the reduction ratio of treated columns determined by substituting the respective material properties $(\rho = 1.40, \rho' = 1.50, V = 40.0, V' = 850, t = 2.0, f = 6.0)$ was estimated to be 0.705.



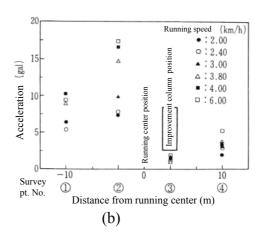


Figure 7. Variation of Acceleration with Speed and Distance from the Vibrating Source

6. CONCLUDING REMARKS

This study presents the current understanding and state-of-practice in using deep mixing technology for vibration impediment. The limited and rare field data from Japan and Sweden is presented to portray the current level of understanding. Measurements performed before and after installation of deep mixed columns under railway embankment at the site in southern Sweden demonstrated that train induced vibrations can be reduced effectively by this method. The complexity of train-induced vibration and high cost of field tests dictates taking advantage of advanced numerical techniques to predict the effect of countermeasures. The numerical solutions with 3-D modeling capabilities have demonstrated effective tools to predict improvement effect of deep mixing as a countermeasure for vibration control. The references provided at the end of this article are aimed to serve as a source for deep mixing technology and vibration impediment issues.

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