

COMPARISON OF COMPLIANCE RESULTS OBTAINED FROM THE VARIOUS WIND FARM STANDARDS USED IN AUSTRALIA

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There are a number of standards and guidelines which are used in Australia for the assessment of wind farm noise, most of which provide different methods for measuring compliance once the wind farm is operational. This paper examines the differences that result when assessing compliance against the various compliance measurement and analysis procedures. Compliance measurements from a thirteen receivers at distances of 300 metres to 3 kilometres from six wind farm sites are used in the analysis. Differences of between 1.9 and 4.3 dB(A) are observed between the highest and lowest assessment results obtained at individual receivers, although this range is reduced to 1.9 - 2.7 dB(A) when L_{Aeq} results that appeared to be influenced by extraneous noise are discarded. These results complement the findings of our other paper which compares predicted levels against the compliance measurement results, and together these papers can be used to compare predictions against wind turbine noise levels measured and analysed using the different methodologies.

INTRODUCTION

In recent years there has been significant growth in wind farm electricity generation across Australia. The current national focus on renewable energy and greenhouse gas emissions reduction is likely to maintain or result in increased growth in this sector.

There are a number of standards and guidelines which are used or are intended to be used in Australia for the assessment of wind farm noise. These include, but are not limited to; the South Australian *Wind Farms Environmental Noise Guidelines 2009* (2009 SA Guidelines) [1], the South Australian *Wind Farms Environmental Noise Guidelines 2003* (2003 SA Guidelines) [2], Australian Standard 4959:2010 [3], New Zealand Standard 6808:2010 [4], New Zealand Standard 6808:1998 [5], and the currently draft *National Wind Farm Development Guidelines* [6].

A detailed discussion of the slightly different approaches used to set noise criteria for wind farms is beyond the scope of this paper, but the standards and guidelines typically set noise criteria for wind farms to be achieved at sensitive receivers as 40 dB(A) or the background noise level + 5 dB(A), whichever is the greater.

Once noise criteria have been established for a proposed wind farm development it is the acoustic engineer's task to provide detailed wind turbine noise level predictions at the noise sensitive receivers around the site. Following the completion of construction, compliance noise measurements are undertaken at the nearest noise sensitive receivers to confirm compliance with the relevant standard or guideline.

It is important that noise levels are accurately predicted at the design stage. Under-prediction of noise levels may result in failure to meet the noise criteria and the expensive shut down of wind turbines, while overly conservative modelling curtails renewable energy generation and reduces the size, and

potentially the financial viability, of wind farm developments.

The standards and guidelines used to assess wind farm developments provide different methods for measuring and analysing operational noise levels at the completion of construction. These differences between the measurement methods result in differences in the measured noise level and can therefore potentially affect whether or not compliance with the noise criteria is achieved.

Compliance measurements from thirteen measurement locations surrounding six wind farm sites are used in the analysis. When selecting data for analysis, particular focus was placed on using measurement data from locations where wind turbine noise was the dominant noise source, to minimise the influence of background noise on the findings. This paper does not seek to recommend a particular compliance monitoring methodology but rather to assess the magnitude of differences that result when assessing compliance measurements using the various measurement procedures. This paper complements the findings of our other paper which is also included in this edition of *Acoustics Australia* [7]. Together they can be used to compare the accuracy of a number of wind turbine noise prediction methods to compliance monitoring results obtained from a variety of compliance measurement and analysis procedures.

STANDARDS USED IN AUSTRALIA

South Australian Wind Farms Environmental Noise Guidelines 2009

The 2009 SA Guidelines were developed by the South Australian Environment Protection Authority (EPA) [1]. The 2009 SA Guidelines require that the $L_{A90,10min}$ noise level is measured over the range of wind speeds from cut-in speed to the speed of the rated power of the turbines at a minimum. The data is to cover at least 2000 intervals, with at least 500 intervals corresponding

to the worst case wind direction. The worst case wind direction is defined as wind directions within 45° of downwind of the nearest wind turbine to the measurement site. The compliance assessment is based on only the data measured under the worst case wind direction – all data from other directions is excluded from the compliance assessment. A polynomial regression analysis is undertaken to determine the measured wind turbine noise level, with correction for the previously measured background noise data applied if required. Where the above method proves unsuitable for compliance checking the 2009 SA Guidelines allow for alternative techniques to be employed, following discussions with the EPA. Suggested alternatives include attended measurements with periodical shutdown of wind turbines if required.

South Australian Wind Farms Environmental Noise Guidelines 2003

The 2003 SA Guidelines [2] were an earlier version of the 2009 SA Guidelines. The 2003 SA Guidelines are still used in some States to assess wind farm noise. Both the 2003 and 2009 SA Guidelines use L_{A90} levels measured under downwind conditions to assess compliance of the wind farm. The most significant difference between the two guidelines is that the 2003 version does not explicitly allow for correction of the measured level for background noise. The increase in measured compliance level that will result from the presence of background noise is not readily quantifiable given the potential for variation of the background noise, so is beyond the scope of this paper. We do not expect any other differences between the compliance measurement methods in these guidelines will result in significant differences in the measured turbine noise level. The two SA guidelines are therefore not separately assessed in this paper.

New Zealand Standard 6808:2010

New Zealand Standard 6808:2010 *Acoustics – Wind farm noise* [4] was recently adopted in Victoria. NZS 6808:2010 expects that at least 10 days (1440 data points) of compliance measurements are undertaken, with data gathered over the range of wind speeds and directions normally expected at the wind farm. The $L_{A90,10min}$ noise level is measured over this 10 day period.

Unlike the 2009 SA Guidelines, there is no specific requirement to exclude data points outside the downwind direction. However, if the initial background noise measurements indicate a significant difference in the pre-construction noise levels under different wind directions or times of day, noise criteria may be set based on particular wind directions or times of day. There is a chance that the pre-construction background noise levels are different under the future downwind direction when compared to the background levels are under other wind directions. If this was the case noise criteria would be set separately for the downwind direction and other wind directions, such that compliance would be assessed under both the downwind direction and all other wind directions. Additionally, there is a chance that the wind that occurs during the compliance measurements is from predominantly downwind directions.

While a downwind assessment might be undertaken under NZS 6808:2010, we have assumed the much more likely

assessment using all wind directions is undertaken for the purposes of our investigation. NZS 6808:2010 provides the site operator with the option of taking attended ‘on/off’ compliance measurements at receivers if appropriate, but a review of the results from on/off testing is not included in this paper.

New Zealand Standard 6808:1998

New Zealand Standard 6808:1998 *Acoustics – The assessment and measurement of sound from wind turbine generators* [5] was used to set noise criteria for new wind farm applications in Victoria until March 2011. The key difference in the compliance measurement method outlined in NZS 6808:1998 (as compared to NZS 6808:2010) is that $L_{A95,10min}$ levels are used rather than $L_{A90,10min}$ levels. Like the 2010 standard, NZS 6808:1998 potentially requires compliance measurements under different wind directions and times of day.

While not intended by the standard, Planning Permits issued for wind farms in Victoria have typically included the requirement that compliance is assessed separately for the “all-time” (24 hours) and night time (10pm – 7am) period. The requirements for downwind, and 90° sector analysis have also been previously included in Planning Permits although this is not specifically required under NZS 6808:1998 [8].

Australian Standard 4959:2010

Australian Standard 4959:2010 *Acoustics – Measurement prediction and assessment of noise from wind turbine generators* [3] has been relatively recently introduced. AS 4959:2010 was the first standard to require that the L_{Aeq} noise level from the wind farm is assessed against the pre-determined noise criteria. It outlines two possible methodologies that might be used for compliance testing, but notes that the method used should be agreed with the Relevant Authority prior to the commencement of testing.

Methodology 1 included in the Standard follows the same approach as the background noise measurements, with approximately 2000 representative measurements to be collected. The standard leaves many assessment decisions, such as the speeds and directions to be assessed, to the Relevant Regulatory Authority, but notes that:

Generally, data collected when the wind direction is from the wind farm to the receiver would be the data of primary interest to the Relevant Regulatory Authority.

For the purposes of our assessment it has been assumed that the Authority has requested that a downwind assessment is undertaken (downwind ±45° as per the SA Guidelines).

In acknowledgment of the difficulty of measuring L_{Aeq} compliance levels directly without contribution from extraneous noise sources, Methodology 1 of the Standard requires the measurement of the L_{A90} noise level, with a numerical addition of 1.5 – 2.5 dB added to each measurement to account for the expected difference between the wind farm L_{Aeq} and L_{A90} levels. Methodology 1 considers that all noise measured at the receiver is the result of noise from the wind turbines, with no allowance provided to correct for background noise. The standard notes that this method is likely to be a conservative method.

Methodology 2 provided by the standard requires the use of attended noise measurements to validate prediction model outputs and therefore compliance with criteria. Our interpretation of the wording in the Standard is that it requires measurements at only one location to validate the noise model for the entire site. However, opinions received from others working in the field of wind farm acoustics suggest that it may have been intended that this Methodology require measurements at either a single receiver, two or three representative receivers, or all of the receivers around the wind farm site to calibrate the noise model.

At least ten 10-minute L_{Aeq} measurements are required both above and below the ‘critical’ wind speed, with the attended measurements to extend to speeds at least 3m/s above and below the ‘critical’ wind speed. Attended L_{Aeq} measurements with the wind turbines turned off may be used to correct for the influence of background noise if necessary. While this paper presents no results from attended measurements we provide some comment on the suitability of Methodology 2 for determining compliance at all receivers around a wind farm.

Draft National Guidelines July 2010

The Draft *National Wind Farm Development Guidelines* [6] were introduced for a 12 month trial in July 2010. The Draft National Guidelines suggest that initially Methodology 1 of AS 4959:2010 is used for compliance measurements. Where compliance is unclear from those measurements and it is suspected this is as a result of background noise, it is recommended that the same measurement procedure is to be followed, but repeated at a ‘secondary location’. The secondary location is a location selected near the receiver that is the same distance from the same wind turbines, where the geographical setting and predicted noise level is the same as the original location, but is further from extraneous noise sources. Where it is not possible or practical to confirm compliance through measurements at a secondary location, attended measurements using Methodology 2 of AS 4959:2010 are recommended. However, it is important to note that the Draft National Guidelines use attended measurements at each problematic receiver, rather than trying to use measurements at one receiver to confirm the accuracy of noise predictions and compliance at other receivers as appears to be required by AS 4959:2010.

In extreme cases where none of the above methods are able to demonstrate that compliance is achieved but the Relevant Authority agrees that compliance is likely to be achieved, the Draft National Guidelines suggest ‘derived point measurements’. Derived point measurements use measurement results at a location closer to the wind farm where noise levels are clearly controlled by wind farm noise to calibrate the noise model.

As the Draft National Guidelines initially follow Methodology 1 of AS 4959 they are not separately assessed in this paper. However, comment on the suitability of the secondary methodologies suggested by the Guidelines is provided.

Summary of Assessment Methods

The key requirements of the various assessment methods considered in our analysis are presented in Table 1. The alternative measurement techniques provided by some standards are not listed separately in Table 1. While the alternative measurement techniques use a different measurement duration or location of measurement, the noise descriptor and wind direction used by the alternative method for assessing wind turbine noise match those used by the primary compliance assessment method of each of the standards.

SITE DESCRIPTIONS

Six wind farms and thirteen measurement sites have been selected for comparison in this paper as the measurements collected at these measurement sites appear to be controlled by noise from the wind turbines across a reasonable wind speed range.

The measurement sites are typically representative of the closest receivers to wind farms in South Australia, although one of the measurement sites was approximately 3 km from the nearest turbine. We note that a number of the measurement sites were not actually in the vicinity of a noise sensitive receiver, which has assisted to reduce the influence of ambient noise on those measurements. Turbine noise levels at the measurement sites were typically in the range of 35 to 40 dB(A), so are representative of most noise exposed receivers adjacent to wind farms where noise represents a design constraint.

For commercial reasons, the names and locations of the

Table 1. Summary of key requirements of compliance assessment methods

Method	Descriptor	Wind direction	Comment
2009 SA Guidelines	L_{A90}	Downwind	Selected as the reference method which other methods are compared to.
2003 SA Guidelines	L_{A90}	Downwind	Similar to above 2009 SA Guidelines, so not assessed separately.
NZS 6808:2010	L_{A90}	All	-
NZS 6808:1998	L_{A95}	All	-
AS 4959:2010	L_{Aeq}	Downwind	Assumed that Regulatory Authority has requested downwind assessment.
Draft National Guidelines	L_{Aeq}	Downwind	Similar to above AS 4959, so not assessed separately.

wind farms have not been disclosed and the wind farms will be designated as Wind Farm A through to F. Based on compliance monitoring conducted at each site, all of these wind farms are in compliance with the environmental noise criteria. A description of each wind farm is presented in the following sections.

Wind Farm A

Wind Farm A involves a line of turbines stretching for about 10 kilometres along the top of a range of hills. The turbines are spaced approximately 400 metres apart from each other. Three noise measurement sites have been considered as part of this comparison and have been designated A1, A2 and A3. Each of the measurement sites are located between 800 and 1000 metres from the nearest turbine, and are situated 50 to 70 metres lower than the base height of that turbine.

Wind Farm B

Wind Farm B also involves a line of turbines stretching for about 10 kilometres along the top of a range of hills. The turbines are spaced approximately 300 metres apart from each other. Four noise measurement sites have been considered as part of this comparison and have been designated B1 to B4. Sites B1, B2 and B3 are located approximately 1,000 to 1,500 metres from the nearest turbine, with B4 located approximately 3,000 metres away. All sites are situated 130 to 200 metres lower than the base height of the nearest turbine.

Wind Farm C

Wind Farm C involves a group of turbines distributed over a flat area of about 20 square kilometres. The turbines are spaced approximately 350 metres apart from each other. Three noise measurement sites have been considered as part of this comparison and have been designated C1, C2 and C3. The measurement sites are located between 300 and 900 metres from the nearest turbine.

Wind Farms D, E and F

At Wind Farms D and E, the turbines are arranged in a line, while the turbines at Wind Farm F are arranged into a group. Only one noise measurement site has been selected for this comparison at each of these Wind Farms as noise levels at all other measurement locations had been controlled by background noise. There is relatively flat ground between the turbines and measurement locations, which are located between 350 and 1200 metres from the nearest turbine.

NOISE MEASUREMENT PROCEDURE

A-weighted $L_{eq,10min}$, $L_{90,10min}$ and $L_{95,10min}$ noise levels from the operational wind farms were logged at each of the measurement sites over a period of three to four weeks. Class 2 noise monitoring equipment was used at each of the sites and the calibration checked both before and after the measurement period to check that no significant drift had occurred. The microphone was located at 1.2 to 1.5 metres above ground and fitted with a 90 mm thick windshield, which was adequate to reduce the influence of wind-induced noise on the measurement [9].

Measurements that were obviously affected by extraneous noise sources or that did not coincide with wind speeds between

the cut-in and cut-out of the turbines were excluded from the analysis. For certain situations, the measurements were filtered based on wind direction when results for specific wind directions were required, e.g. for the 2009 SA Guidelines. Following the removal of data points, between 2000 and 4000 data points remained at the various measurement sites for the situations where all wind directions were being considered. For those situations where only a single wind direction $\pm 45^\circ$ was considered, between 200 and 1000 data points remained at the various measurement sites. Where less than 500 data points remained at a particular wind speed, these were confined mainly to the small range of wind speeds where site measured sound power data was available.

The measured noise levels were correlated with wind speeds for the period, measured at the most representative hub height meteorological mast or nearest turbines to the measurement site. A single "measured" noise level value for each integer wind speed was then determined by fitting a polynomial regression line to the data.

A significant issue that can affect measurement results from operational wind farms is the contribution of the background noise environment. While this can be somewhat overcome by subtracting the measured pre-construction noise levels, Delaire and Walsh [10] showed this method is susceptible to error as background noise levels can change across seasons and years. The pre- and post-construction measurement locations may also be different, another possible inaccuracy with this method. To address this, each measurement site was selected such that it was as far away as possible from potential sources of background noise (e.g. trees, occupied dwellings), and such that the noise level at the site was typically controlled by turbine noise. In addition, only wind speeds where the L_{A90} noise level appears to be consistently controlled by turbine noise were considered in our analysis. These wind speeds have been selected based on analysis of the measurement data and supported by observations made on site during the measurements. Wind speeds where there was a significant spread in the measured noise levels were excluded, as observations on site indicated this variation was the result of extraneous noise sources affecting measured levels.

As an example, Figure 1 presents measurement results for Site B3, indicating a wind speed range of 4 to 12 m/s where the measured noise level is controlled by turbine noise. This is evident due to the small spread of the measurement data when compared to wind speeds above 12 m/s where background noise causes significant variation between measured noise levels at the same integer speed. At lower wind speeds, there are also a number of measurements where the turbine clearly cut-out due to low wind speed during the measurement period. These have been excluded from further analysis. For each measurement site, between three and six integer wind speeds were identified as being in the turbine-controlled wind speed range.

The change in measured noise levels with wind speed across this wind speed range correlated almost precisely with the change in sound power levels for the turbines, an indication that the noise levels were controlled by noise from the turbines. This is discussed in more detail in Ref. [7].

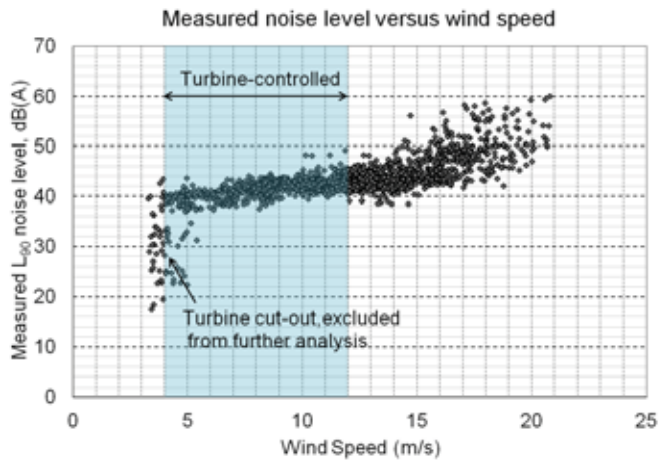


Figure 1. Example of measured noise levels versus wind speed with turbine-controlled wind speed range

RESULTS

The compliance noise level measured using the 2009 SA Guidelines was selected as a reference level, against which the results from all other compliance measurement methods were compared. The 2009 SA Guidelines use the worst case wind direction and the L_{A90} noise level, which is expected to make them less susceptible to variation than some other methods. The use of the downwind directions should, in practice, provide a more repeatable compliance measurement as the result will not be influenced by variations in the distribution of wind directions that occur during the compliance measurement period. Additionally, L_{A90} levels should be less susceptible than L_{Aeq} levels to the influence of short term extraneous noise.

In support of this supposition, compliance measurements were recently repeated at one of the sites in this study, almost two years after they were first assessed using the 2009 SA Guidelines. The variation in the measured compliance level was less than 1 dB(A) over the entire range of wind speeds where the noise level appeared to be turbine-controlled. This demonstrates the repeatability of the 2009 SA Guidelines compliance measurement method when used at locations not influenced by extraneous noise.

Table 2 summarises the average difference in compliance measurement results achieved between the tested methods at each site. To determine the difference between the reference method (chosen to be the 2009 SA Guidelines) and other compliance measurement methods, the wind turbine noise level was determined using each of the compliance assessment methods for all turbine noise controlled wind speeds. At each site, the 2009 SA Guidelines noise level was then subtracted from the noise level determined using the other compliance measurement method at each integer wind speed, to give a difference between the methods at each turbine controlled wind speed. There was typically little difference in the result with wind speed, so these differences were averaged across all turbine controlled wind speeds to give an average difference between the 2009 SA Guideline and the other compliance measurement method.

We note that Method 1 of the AS 4959:2010 requires the measurement of L_{A90} levels, with a numerical adjustment applied to account for the likely difference between the L_{A90} and L_{Aeq} level. As it is assumed that the AS 4959:2010 assessment uses only downwind directions, the required AS 4959:2010 assessment would match the 2009 SA Guidelines assessment, except that the AS 4959:2010 assessment would

Table 2. Compliance level measured using the different compliance methods, relative to the 2009 SA Guidelines (dB(A))

Site	Difference in level relative to 2009 SA Guidelines (dB(A))		
	NZS 6808:1998	NZS 6808:2010	AS 4959:2010
A			
A1	-1.5	-1.1	+2.8
A2	-1.5	-1.0	+2.5
A3	-2.0	-1.5	+1.9
B			
B1	-1.0	-0.7	+1.7
B2	-0.7	-0.4	+1.2
B3	-1.1	-0.7	+1.5
B4	-1.2	-0.7	-
C			
C1	-0.5	-0.2	+1.6
C2	-0.7	-0.4	+1.4
C3	-0.7	-0.4	+1.3
D, E and F			
D1	-	-0.3	+1.1
E1	-0.9	-0.5	+1.9
F1	-1.4	-1	-
Mean Difference	-1.1	-0.7	+1.7
Standard Deviation	0.4	0.4	0.5

require the numerical addition of 1.5 to 2.5 dB(A) to the 2009 SA Guidelines result. Rather than rely on the numerical adjustment provided by the Standard, our AS 4959:2010 assessment is based on measured L_{Aeq} levels instead. The calculated difference between the AS 4959:2010 result and the 2009 SA Guidelines result provides the actual difference between the L_{Aeq} and L_{A90} levels.

No difference is provided between the 2009 SA Guidelines and NZS 6808:1998 for site D1 as L_{A95} levels were not measured at that site. No difference is provided between the 2009 SA Guidelines and AS 4959:2010 for sites B4 and F1 as L_{Aeq} levels at those locations were clearly significantly controlled by short term extraneous noise. Results for the 2003 SA Guidelines and Draft National Guidelines are not reported separately as they share key compliance measurement requirements with the 2009 SA Guidelines and AS 4959:2010 respectively.

Table 2 indicates that the application of other wind farm standards used in Australia results in levels up to 2.0 dB(A) lower, and 2.8 dB(A) higher than respective results obtained through application of the 2009 SA Guidelines. However, as later discussed, the 2.8 dB(A) difference between the 2009 SA Guidelines and AS 4959:2010 at site A1 is believed to be exaggerated by extraneous noise.

Discussion of L_{A90} and L_{A95} Results

It is observed that measurements undertaken using NZS 6808:1998 provide the lowest compliance levels, with a mean level 1.1 dB lower than the 2009 SA Guidelines and a range of results between 0.5 and 2.0 dB lower than the 2009 SA Guidelines. However, we note that this does not necessarily translate to a 0.5 to 2.0 dB less stringent end result at the residences. Existing background noise levels used to determine noise criteria would also be measured using the L_{A95} assuming that the NZS 6808:1998 method had been applied throughout the planning phase as well as during the compliance monitoring phase. Noise criteria determined based on the background $L_{A95} + 5$ dB approach would be more stringent than those determined using an L_{A90} level.

The variation in differences between noise levels measured under the 2009 SA Guidelines approach and NZS 6808:1998 approach was 1.5 dB (differences of between -2.0 and -0.5 dB). This result appears to be attributable to the combination of the difference in wind directions used for the assessments, turbine layout, and difference between the L_{A95} and L_{A90} levels. The difference in L_{A95} and L_{A90} is 0.3 to 0.5 dB, as provided by comparison of the NZS 6808:1998 and NZS 6808:2010 results in Table 2 (the only difference between these being the use of L_{A90} rather than L_{A95} in NZS 6808:2010). The remaining variation in levels is attributable to different proportions of downwind measurements in the total measurement period, and layout of turbines on site.

Discussion of L_{Aeq} Results

The AS 4959:2010 results provide the highest measured levels across all measurement sites. The comparison of the AS 4959:2010 and SA Guidelines methods provides the average difference between L_{A90} and L_{Aeq} levels across the

measurement sites. From site observations at the base of a turbine it might have been expected that locations close to turbines would experience greater differences between L_{A90} and L_{Aeq} levels, due to the blade passing of a single close turbine being more noticeable than the blade noise on a group of distant turbines. However, no discernible relationship between distance and difference in L_{A90} and L_{Aeq} results were observed during our analysis. Rather, the sites where both site observations and plots of noise level versus wind speed suggested greatest influence of ambient noise correspond to the sites with highest difference between the L_{A90} and L_{Aeq} levels.

While it is difficult to quantify the influence of ambient noise on the measurement sets, site observations and the scatter of the L_{Aeq} data points (including at speeds below turbine cut-in) suggest that the L_{Aeq} results at sites A1, A2, A3, E1 and possibly also B1 have been noticeably increased by ambient noise. If these sites which are believed to be affected by significant extraneous noise (A1, A2, A3 and E1) are excluded from the data set the mean difference between L_{A90} and L_{Aeq} across the seven remaining sites is only 1.4 dB(A), with the range of results obtained using the various wind farm standards up to 2.0 dB(A) lower, and 1.7 dB(A) higher than those achieved using the 2009 SA Guideline.

The average difference between L_{A90} and L_{Aeq} results of 1.4 dB(A) is less than the suggested correction of 1.5 to 2.5 dB(A) previously provided by ETSU [11] and adopted by AS 4959:2010. Our results suggests that L_{A90} levels should be increased by no more than the minimum required by AS 4959:2010, which is 1.5 dB(A). It is possible that the difference between our findings and those reported in ETSU is the result of extraneous noise during the ETSU assessment, or measurements undertaken at very close distances to a single turbine where modulation of the noise may have been greater.

Differences of between 1.9 dB(A) and 4.3 dB(A) (at B2 and A1 respectively) are observed between the highest and lowest assessment results obtained at individual receivers, although this range is reduced to 1.9 to 2.7 dB(A) (at B2 and B1 respectively) when L_{Aeq} results at the four measurement sites that appeared to be most significantly influenced by extraneous noise are discarded.

Finally, we note that the AS 4959:2010 Methodology 1 does not allow for the correction of L_{A90} compliance measurements for background noise, which the standard notes is a conservative approach. The lack of the ability to correct for the contribution of background noise when using this method will further increase the difference between the SA Guidelines and AS 4959:2010 results. There is potential for the inability to correct for the significant background noise at a typical compliance measurement site to be sufficient to incorrectly indicate non-compliance with criteria.

Comment on Alternative Measurement Techniques

There are a number of alternative compliance measurement techniques proposed by the various standards including; attended on/off measurements, long term measurements at 'secondary locations' adjacent to residences, long term measurements at 'derived locations' between the turbine and

residence with a correction applied for the predicted difference in noise level between the derived location and residence, and attended measurements at one residence to calibrate a noise model for the site.

Of all the alternative compliance measurement techniques proposed by the standards, the authors most prefer the use of measurements at a 'secondary location' which is a location selected where turbine noise levels are expected to be the same as at the residence but background noise levels are expected to be much lower.

In practice it is not always practical to place a noise logger in a 'secondary location' where the terrain and distance to all turbines match those at the receiver. Where it would be necessary to place a logger slightly closer or further from the turbines we suggest this is preferable (with a small correction applied for the slight predicted difference in noise level), rather than use attended measurements gathered over a limited range of conditions.

The authors demonstrate there is a consistent difference between the measured and ISO 9613-2 ($G=0$) [12] modelled results at receivers scattered across different wind farm sites, provided that the terrain between the turbines and receivers is consistent [7]. We therefore also support the use of logging at a location slightly removed from a receiver i.e. in a 'derived location'. The correction applied for the difference in location should be determined using the ISO 9613-2 ($G=0$) prediction method, and the distance between the measurement location and residence should be always be minimised as far as is practical. Our other paper demonstrates that all of the noise models currently in use do not account for the influence of topography on noise propagation. If a 'derived location' is used, it is critical that significant differences in terrain between the derived measurement location and residence are avoided.

Where there is significant background noise, the above two methods will provide a better indication of turbine noise than the primary compliance measurement methods currently used by the various Standards and Guidelines. The primary measurement methods involve taking measurements significantly influenced by background at receivers and then correcting them through subtraction of historical L_{A90} levels or alternatively measuring at the receiver and ignoring the presence of the significant extraneous noise.

The suitability of attended measurements for determining wind farm noise levels at an individual location has not been examined in this paper but we anticipate they would provide acceptable results provided that the sample size is sufficiently large. It may be simpler and less labour-intensive to take long term measurements at a secondary or derived location than it is to take a large number of attended measurements at a location influenced by background noise.

Our interpretation of the alternative compliance technique provided by Methodology 2 of AS 4959:2010 is that it requires attended noise measurements at one noise sensitive receiver to validate prediction model outputs and therefore compliance with criteria at the other receivers. We therefore have concerns regarding the suitability of Methodology 2 for checking compliance across a wind farm site. Using the receivers at Wind farm A as an example; sites A2 and A3 are at a very similar

distance but on opposite sides of a small group of turbines. The terrain between the turbines and two measurement sites varied greatly, which resulted in a difference in the measured noise level between the two sites being 5.9 dB(A). However, as the available models do not account for the influence of terrain, the very similar distances to the turbines resulted in predicted noise levels at the two sites being almost identical. If Methodology 2 had been applied using attended measurements at Site A2 to calibrate the noise model the compliance level determined for Site A3 would have been almost 6 dB(A) too low, due to the lack of influence of terrain on the predicted noise levels. We therefore strongly suggest that Methodology 2 should only be used for receivers sharing similar terrain, and this method in the Standard should be revised to reflect this requirement as soon as practical.

CONCLUSIONS

A comparison of the compliance results obtained from the various wind farm standards used in Australia has been undertaken. Noise measurements collected from 13 measurement sites around six different wind farms have been used during our assessment. Each measurement site selected for this analysis exhibited wind speeds where noise measurements were clearly controlled by wind turbine noise, with only data from those speeds assessed.

The compliance noise level measured using the 2009 SA Guidelines was selected as a reference level, against which the results from all other compliance measurement methods were compared. The measurement results obtained using the other wind farm standards are at levels up to 2.0 dB(A) lower, and 1.7 dB(A) higher than respective SA Guideline results, when L_{Aeq} results believed to be increased by ambient noise are discarded.

Application of NZS 6808:1998 results in the lowest measured compliance levels, with mean level 1.1 dB lower than the SA Guideline. This result is attributable to both the use of an L_{A95} descriptor rather than L_{A90} , and assessment over all wind directions rather than just downwind conditions. When compared to the NZS 6808:1998 standard, the new NZS 6808:2010 standard provides compliance results approximately 0.4 dB(A) higher. AS 4959:2010 provides the highest measured compliance results, with mean difference between the L_{A90} and L_{Aeq} found to be 1.4 dB when several outlier sites which were believed to have been influenced by extraneous noise are excluded.

This paper does not seek to recommend noise measurement descriptors or wind directions that should be used to assess wind farm noise, but rather identifies the differences in measured noise levels achieved by the various measurement techniques. Together with the findings in Ref. [7], the accuracy of a number of noise prediction methods to compliance results obtained from a variety of compliance measurement approaches can be compared. Some commentary has been provided on the range of alternative compliance measurement methods used in Australia. The authors strongly suggest that Methodology 2 of AS 4959:2010 is revised as soon as is practical, given the modelling errors that result from variations in topography between the turbines and receivers.

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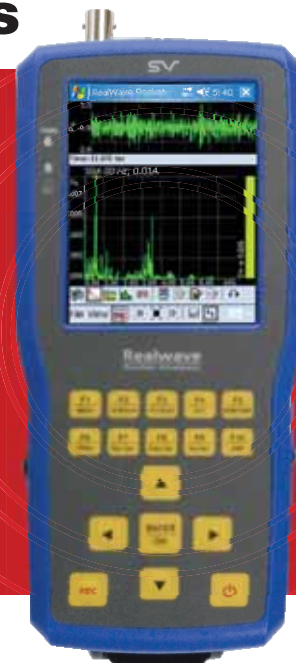
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