

Use of ISO measurement uncertainty guidelines to determine uncertainties in noise & vibration predictions and design risks

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ABSTRACT

There are many standards and guidelines that can be used to assist in expressing measurement uncertainty, however there aren't many that can assist in determining uncertainties in noise predictions and design risks. A common way that noise and vibration engineers deal with prediction uncertainties is to assume an uncertainty of +/- X dB in their modelling or to simply add a safety factor of +Y dB to their design. This paper shows how international guidelines were used on some recent rail transport infrastructure projects to quantify the uncertainties in noise predictions and to establish the level of design risk associated with those uncertainties. Prediction uncertainties were determined from the methodologies described in the International Standard ISO/IEC Guide 98-3 'Guide to the expression of uncertainty in measurement' (GUM) and by establishing an uncertainty budget for each part of the ground-borne noise and prediction process (source, path and receiver). A Monte Carlo simulation was also undertaken with 100,000 iterations to provide an estimate of the standard uncertainty. This was compared with the GUM approach and gave similar results.

1. INTRODUCTION

It is important to recognise that all scientific predictions (and measurements) contain some degree of error. Therefore, when predicting the potential impacts from something as complex as ground-borne noise and vibration from underground rail operations, there are many errors or uncertainties that will occur with predictions.

On projects where there is limited or only high-level information relating to source, path and receiver components, the uncertainties associated with predicting noise and vibration levels can be quite large. For example, when predicting airborne noise from a well understood sound source located in a reasonably uncomplicated situation and within acoustically benign surroundings, modelling uncertainties of ± 3 dB(A) for near predictions and ± 5 dB(A) for far predictions are not uncommon. However, when predicting vibration and ground-borne noise propagation in more complex situations such as through a solid medium like the ground and then the transmission of vibration regeneration as noise inside buildings, uncertainties of up to 10 dB(A) are often reported in literature and by many acoustic consultants.

Such simplistic and somewhat ad hoc estimates and approaches are not well founded quantitatively, and can be costly to a project should such uncertainties be added to prediction levels in the form of engineering margins or safety factors to reduce risks of non-compliance.

On recent underground railway tunnel projects, a quantitative approach was used with the aim of improving estimates of prediction uncertainties and to better advise the design teams of the level of design risk associated with the predictions. Field measurements were also utilised to reduce the uncertainty associated with ground-borne noise and vibration predictions. Guidance was taken from International Standard ISO14837-1:2005, which sets out key factors to be considered when predicting ground-borne noise and vibration for rail operations and provides guidance on rail noise and vibration modelling methods.

This paper focuses on the results and outcomes at a representative receiver location which is selected to establish and illustrate the uncertainties in modelling predictions. The combined standard uncertainty at this location was calculated for the source parameters, the path parameters and the receiver parameters. The combined standard uncertainty for the entire prediction path was then calculated. The outcome of these calculations indicated that the predicted ground-borne noise levels are expected to lie within ± 3.9 dB(A) of the mean with a design confidence of one standard deviation (or 84% confidence). With the application of appropriate coverage factors, wider confidence levels can be predicted and the associated design risk evaluated based on quantitative information.

1.1 Railway Ground-borne Noise and Vibration

Ground-borne noise and vibration (GBNV) modelling was undertaken for some recent railway tunnel projects, based on the guidance contained in International Standard ISO14837-1:2005. The standard provides

guidance in relation to the key factors to be considered when predicting GBNV for rail operations and guidance on modelling methods. Three key factors are identified in the propagation of GBNV, and comprise:

1. source vibration levels occurring at the wheel-rail interface and supporting track form,
2. vibration transferred between the tunnel and the ground surface via the surrounding ground, and
3. vibration levels occurring within the building and associated ground-borne noise levels.

For underground railways, vibration is transmitted through the track structure, through the ground mass and into building structures. This vibration has the potential to be perceptible to building occupants as tactile vibration but is usually manifested as ground-borne noise.

The extent of vibration is influenced by several physical aspects such as: mass of train (axle load and unsprung mass); train speed and length; condition of rail surface (e.g. alignment, roughness and defects such as corrugations etc.); condition of wheels (e.g. roughness, flats or other wheel defects etc.); type of track structure and form (e.g. stiffness or softness of rail track bed and fasteners, tunnel type, etc.); ground type between tunnel and receiver buildings; distance between tunnel and receivers, tunnel depth and construction type of receiver buildings.

Table 1: Modelling Parameters and Description of Uncertainties

No.	Modelling Parameters	Description of Uncertainty
<i>Source Parameters</i>		
1	Source level measurement resolution	error associated with rounding up or down measurement results to the nearest decimal place
2	Variation in source vibration levels between sites	range based on measurement results at several locations in similar rail tunnels
3	Measurement equipment uncertainties	error associated with measurement instruments used in the source vibration measurements
4	Measured speed variation	accuracy of train speed measurements undertaken for the source vibration measurements
5	Predicted rail roughness variation	assumed +/- 2.5dB variation in rail roughness compared with levels compliant with ISO 3381 [8]
6	95 th percentile correction	assumed standard deviation of source variance for 95 percent of train passbys – assumed between 2 to 4dB. For this project, noise compliance was assessed based on the 95 th percentile (highest 1 in 20) passby noise level.
7	Logarithmic summation errors when calculating overall dB(A) levels	previous measurements indicate logarithmic sum of 1/3 octave band spectra measured in the field are on average 0.5dB(A) higher than low-frequency band limited $L_{Amax,slow}$ levels, but found to vary from 0 to 1dB(A)
<i>Path Parameters</i>		
8	Train speed variation	assumed speed variation of actual train speeds +0%, - 5%
9	Train speed relationship	assumed variation from 15 log to 25 log [Hassan O.A.B, 2006], [Nelson P, 1987] & [US FTA, 2006]
10	Fastener corrections	assumed +/- 2dB variation in calculation of insertion loss of proposed fasteners for the project
11	Stiffness variations	assumed variation in overall track stiffness due to production tolerances

12	Rail vehicle unsprung mass variation	attenuation varies depending on unsprung mass of rail vehicles proposed to be used on the line
13	Frequency band corrections	potential error if path correction spectra is shifted +/- 1/3 octave band
14	Ground conditions from source to receiver	variation in excess attenuation values per 10 m distance between tunnel and receiver on ground surface
15	Attenuation calculation method - source to receiver	error associated with calculation method of attenuation between source and receiver – two different methods utilised to estimate range

Receiver Parameters

16	Distance calculation error	from ground contour maps, assumed accuracy of +/- 1m vertically at receiver locations
17	Coupling losses & Building amplifications	standard deviation of coupling loss and amplification values determined from field measurements at several locations
18	Conversion from Vibration to Noise levels	based on [Nelson P, 1987] and [US FTA, 2006]

1.2 Modelling Parameters & Uncertainties

The rail GBNV standard [ISO 14837-1:2005] identifies three primary methods for predicting ground-borne noise and vibration. These include parametric models (algebraic and numerical solutions), empirical models of various types, and semi-empirical models, which involve a combination of parametric and empirical components.

The modelling for this project was based on a combination of measurement data obtained from an underground railway line with similar ground conditions, with interpolation and extrapolation of these results for situations where different source, ground or receiver conditions occurred. Where corrections were required, these were calculated using a variety of parametric and empirical methods. The GBNV prediction algorithms had been previously validated via field measurements on another underground rail scheme.

The calculated GBNV along an underground rail corridor are based on numerous parameters and assumptions considered during the design phase. Some parameters can be easily quantified with a good degree of certainty, while other parameters can only be estimated based on very little available data and information, causing these to have lower certainty.

For the subject rail tunnel, the parameters quantified and used in the predictions are presented in Table 1. An estimate of the prediction uncertainties was undertaken to quantify and advise the design team of the level and range of design risks that are associated with the rail GBNV predictions.

It is important to recognise that all scientific predictions (and measurements) have some degree of error. Therefore, when predicting the potential impacts from GBNV from underground rail operations, there are errors or uncertainties that will occur with predictions. Prediction uncertainties were determined based on the methodologies described in the GUM.

For each modelling input parameter (or source of uncertainty), an estimate of the likely range (minimum and maximum) of values was made based on field measurement results, published data and engineering judgement. An uncertainty budget was established for each part of the ground-borne noise and prediction process (refer Table 1), based on guidance in Reference [Craven N J and Kerry G, 2007].

2. UNCERTAINTY, CONFIDENCE INTERVALS AND COVERAGE FACTORS

This paper examines how prediction uncertainties can be determined even with undertaking complex GBNV predictions. To illustrate the methodology and procedure followed, an example receiver above the railway tunnel was selected to establish uncertainties in the modelling predictions.

The GUM provides detailed guidance on how to calculate the U_{xx} , the differences between Type A (statistical) and Type B (any other non-statistical means) evaluations, distribution types (e.g. normal, triangular, rectangular, etc.), ranges, etc., and how to evaluate the combined uncertainty.

A Type A uncertainty analysis is typically based on determining the standard deviation (standard uncertainty) of measurement results. A Type B uncertainty analysis involves estimating the uncertainty of the input parameter from published data, calculations, engineering judgement or common sense. Type A and Type B analyses are considered in this example.

For some Type B evaluations, it is only possible to estimate the upper and lower limits of uncertainty. It may then be assumed that either the value is equally likely to fall anywhere in between, (i.e. a rectangular or uniform distribution) or that there is a greater chance that the value will fall close to the mean of the possible data range (i.e. a normal or triangular distribution). Other distribution types are also possible.

2.1 Uncertainty Budgets

A summary of the uncertainty budget calculations is provided in Table 2. For each modelling input parameter, an estimate of the standard uncertainty (uncertainty contribution) has been made.

For some input parameters (e.g. speed variations and unsprung mass), the minimum and maximum assumptions which are utilised to establish the range in possible values must be converted into decibels before the uncertainties can be combined. Thus a 5% change in the accuracy of train speed measurement was determined to be equivalent to a 0.4dB change in GBNV levels.

Individual standard uncertainties can be combined validly by 'summation in quadrature' (also known as 'root sum of the squares'), which is called the combined standard uncertainty and denoted by u_c :

$$\text{Combined uncertainty} = \sqrt{a^2 + b^2 + c^2 + \dots \text{etc.}} \quad (1)$$

The approach of summing the uncertainties works well where calculations of prediction results involve the summation of a series of values. For example, when calculating GBNV levels, calculations begin with source vibration 1/3 octave band spectra to which corrections are added or subtracted to derive predicted levels at receiver locations. In this and similar cases, parameter uncertainties are treated equally and are unweighted. For cases where calculations involve the multiplication, division, power or logarithm of values (e.g. when adding vibration or noise components to arrive at total levels), relative or fractional uncertainties must be used in order to weight the effect of parameter uncertainties on the combined standard uncertainty (refer to GUM).

2.2 Confidence Intervals and Coverage Factors

Uncertainty is the measure of dispersion or variance that may be expected with a claimed performance value, often represented by the term U_{xx} . The subscript 'xx' means a xx% confidence interval. It represents the estimated range in which the true value lies for xx out of 100 repeated events, e.g. a U_{95} of 5 dB indicates that the true value is expected to be within ± 5 dB of the estimates provided for 95% of all observations.

Once the combined standard uncertainty is determined, it may be required to re-scale the result. The combined standard uncertainty may be thought of as equivalent to 'one standard deviation' (1σ), but it may be preferred to have an overall uncertainty stated at another level of confidence. This re-scaling can be done using a coverage factor, k . Multiplying the combined standard uncertainty, u_c by a coverage factor gives a result which is called the expanded uncertainty, usually shown by the symbol U , i.e. $U = ku_c$. A coverage factor $k=2$ results in a confidence level of 95%. The most common level of preferred confidence for acoustic predictions often lies between 68% ($\pm 1\sigma$) and 95% ($\pm 2\sigma$), which can be referred to as having a coverage factor of 1 and 2, respectively.

3. UNCERTAINTY CALCULATIONS

3.1 Uncertainty Predictions based on GUM

For each parameter used in predicting project GBNV levels, an estimate of the standard uncertainty (uncertainty contribution) has been made based on the methodologies described in the GUM. Table 2 presents a summary of the uncertainty calculations.

Table 2 – Uncertainty Calculations

Parameter	Assumptions		Half Range or Standard Deviation dB(A) - c_i	Probability Distribution Type	Distribution Divisor ($1/u_i$) Normal 1σ Rectangular $\sqrt{3}$ Triangular $\sqrt{6}$	Uncertainty Contribution $c_i u_i$ dB(A)	Uncertainty Squared, $(c_i u_i)^2$
	Min	Max					
<i>Source Parameters</i>							
Measurement equipment	-0.4dB	0.4dB	0.4	Normal	1.0	0.4	0.2
Vibration source level variations	min Vib	max Vib	3.1	Rectangular	1.7	1.8	3.2
Measured speed	-5%	5%	0.4	Rectangular	1.7	0.3	0.1
Predicted rail roughness	-2.5dB	2.5dB	2.5	Rectangular	1.7	1.4	2.1
95th percentile	3.3dB	6.6dB	1.6	Rectangular	1.7	0.9	0.9
Log sum errors when calculating	-1.0dB	0.0dB	0.5	Triangular	2.4	0.2	0.0
<i>Combined Standard Uncertainty - Source</i>							2.5dB(A)
<i>Path Parameters</i>							
Train speed variation	-5%	0%	0.3	Normal	1.0	0.3	0.1
Train speed	15log	25log	0.3	Rectangular	1.7	0.2	0.0
Fastener corrections	-2dB	2dB	2.0	Triangular	2.4	0.8	0.7
Stiffness variations	-15%	15%	1.4	Triangular	2.4	0.6	0.3
Rail vehicle unsprung mass	950kg	750kg	0.8	Rectangular	1.7	0.4	0.2
Frequency band	move spectra 1/3 octave		2.3	Rectangular	1.7	1.3	1.8
Ground conditions from source to	2dB per 10m	1dB per 10m	1.3	Rectangular	1.7	0.8	0.6
Attenuation calculation	Method 1	Method 2	0.9	Rectangular	1.7	0.5	0.3
<i>Combined Standard Uncertainty - Path</i>							2.0dB(A)
<i>Receiver Parameters</i>							
Distance calculations	-1m	1m	0.2	Rectangular	1.7	0.1	0.0
Building coupling losses / amplifications	-1.8dB	1.8dB	1.8	Normal	1.0	1.8	3.2
Conversion from	-31dB	-27dB	2.0	Rectangular	1.7	1.2	1.3
Resolution (nearest)	-0.5dB	0.5dB	0.5	Rectangular	1.7	0.3	0.1
<i>Combined Standard Uncertainty - Receiver</i>							2.2dB(A)
Combined Standard Uncertainty from GUM [1]						$u(L_m) = \sqrt{\sum_1^n (c_j u_j)^2}$	3.9dB(A)
Expanded Uncertainty for U68 (68% confidence)							k = 1 3.9dB(A)
Expanded Uncertainty for U95 (95% confidence)							k = 2 7.8dB(A)

The combined standard uncertainty is calculated to be 2.5dB(A) for the source parameters, 2.0dB(A) for the path parameters and 2.2dB(A) for the receiver parameters. The combined standard uncertainty for the entire prediction path is calculated to be 3.9dB(A). This indicates that the predicted ground-borne noise levels are expected to lie within $\pm 3.9\text{dB(A)}$ [$\pm 1\sigma$] of the predicted levels with 68% confidence and within $\pm 7.8\text{dB(A)}$ [$\pm 2\sigma$] of the predicted levels with 95% confidence.

For compliance with specifications or design noise targets, predictions with confidence intervals of 84% (+1 σ) or 95% (+1.64 σ), are commonly found in standard Normal Distribution tables, for example [Walpole R & Myers H, 1993]. So, there is:

- 84% confidence that the true level will be below the predicted level plus 1 σ [i.e. plus 1 x 3.9 = 3.9 dB(A)]
- 90% confidence that the true level will be below the predicted level plus 1.28 σ [i.e. plus 1.28 x 3.9 = 5.0 dB(A)]
- 95% confidence that the true level will be below the predicted level plus 1.64 σ [i.e. plus 1.64 x 3.9 = 6.4 dB(A)].

3.2 Uncertainty Predictions based on Monte-Carlo Simulation

To validate the combined standard uncertainty of the predictions presented in Table 2, a Monte Carlo simulation was performed.

For each modelling input parameter, a pseudo-random number was generated within a spreadsheet and the corresponding prediction error was determined based on the half range or standard deviation, and associated probability distribution function (normal, rectangular or triangular). For each iteration, the total prediction error was calculated by arithmetically summing the prediction errors associated with each modelling input parameter. This process was repeated for 100,000 iterations.

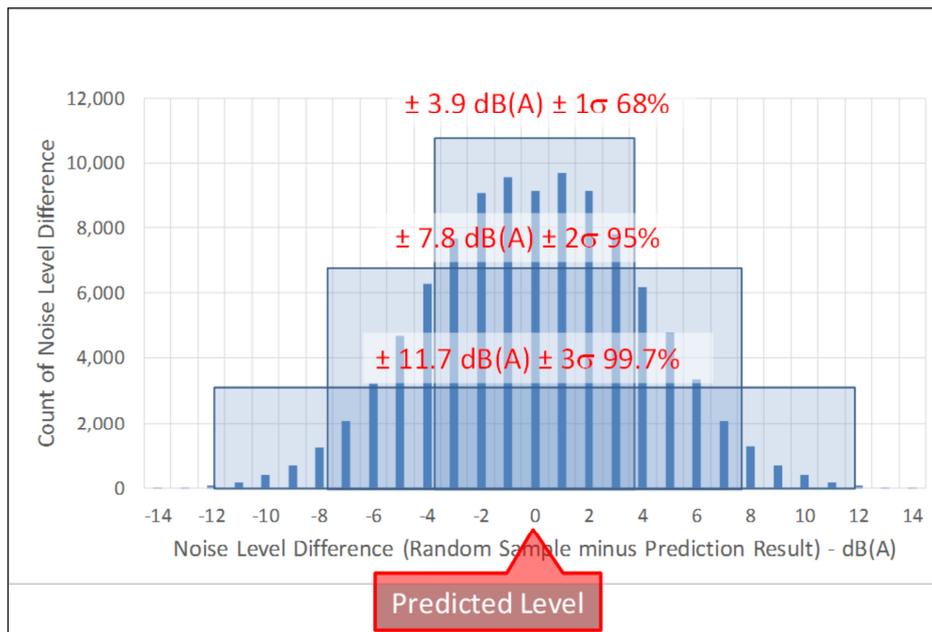


Figure 1 – Monte Carlo Analysis Results

The results of this analysis yielded a standard deviation (combined standard uncertainty) of 3.9dB(A) in the prediction errors (as shown in Figure 1), consistent with the GUM analysis method in Table 2.

4. METHODS USED TO REDUCE MODELLING UNCERTAINTY

Regarding the example uncertainty budget calculations in Table 2, the overall uncertainty can be reduced most effectively by focusing on the modelling input parameters with the largest uncertainty. For the rail projects selected for this paper, the GBNV input parameters found to have the largest uncertainty were: vibration source levels; rail roughness levels; ground conditions / attenuation between source and receivers; building coupling

losses / amplifications; the vibration spectrum shape; and the algorithm conversion of vibration to noise. Field vibration and noise measurements from the subject project and other similar projects were reviewed to assist with reducing the uncertainty of some of these key parameters:

- **Vibration Source Levels:** The variation in source vibration levels at otherwise identical measurement sites with similar track forms were established based on measurement data from an existing railway tunnel. One-third octave band vibration measurements of multiple train passbys were undertaken at multiple locations with known track forms, rolling stock and train speeds. Corrections to the measured vibration levels were made to account for minor differences in the proposed track forms, rolling stock and speeds. The uncertainty associated with these corrections form part of the uncertainty predictions.
- **Rail Roughness Levels:** The typical variation in rail roughness was investigated via a review of rail roughness measurements undertaken on a comparable railway scheme. Within the wavelength range critical to ground-borne noise (greater than 100mm for train operations less than 100km/h), the measured rail roughness levels were typically lower than the rail roughness limit spectrum in ISO 3381-2005 and ISO 3095-2005 at all locations. For modelling, it was assumed that the rail roughness levels would be maintained to these standards or better throughout the life of the rail system and that this would be achieved via the periodic measurement of rail roughness and acoustic rail grinding.
- **Ground conditions / attenuation:** Between the tunnel and ground surface, vibration attenuation occurs due to two primary factors: geometric spreading (via body waves) and excess attenuation (due to material damping). For train vibration (where the length of the train is large compared with the propagation distance), vibration levels attenuate in a cylindrical pattern at a rate of 3 dB per doubling in distance [Hassan OAB, 2006; Nelson P, 1987; & US FTA, 2006]. Additional losses due to material damping are frequency dependent, with greater losses occurring at higher frequencies (smaller wavelengths). Excess attenuation values were determined from transfer mobility measurements and vibration measurements above project tunnels during tunneling construction works. Excess attenuation values at several locations across all data sets were found to be generally comparable and were adopted for modelling purposes.
- **Building Coupling Loss / Amplification and Conversion Factors from Vibration to Noise:** Attended noise and vibration measurements were conducted at multiple sensitive receiver locations near the project tunnels. The purpose of the measurements was to quantify: vibration propagation between tunnels and ground surface; coupling loss and amplification (difference in ground-borne vibration levels outside building and floor vibration levels inside building), and conversion of floor vibration levels to audible noise. A statistical approach, based on the measurement results at multiple locations was utilised to calculate the standard deviation of the results.

The uncertainty budget calculations in Table 2 include the benefits of the above field test inputs.

5. MODELLING UNCERTAINTY RESULTS AND OUTCOMES

Assessment of the modelling uncertainty using a quantitative approach based on GUM provides the additional benefit of quantifying the probability (confidence level) of the prediction uncertainty. Rather than simply stating that the prediction uncertainty is accurate to $\pm 5\text{dB}$ or $\pm 10\text{dB}$, the prediction uncertainty based on GUM for the selected example can be stated as follows:

- the predicted ground-borne noise levels are expected to lie within $\pm 3.9\text{dB(A)}$ [$\pm 1\sigma$] of the predicted levels with 68% confidence, or within $\pm 7.8\text{dB(A)}$ [$\pm 2\sigma$] of the predicted levels with 95% confidence;
- by adding an engineering margin of one standard deviation [3.9 dB(A)] to the predicted noise level, the probability of the actual (or true) noise level being less than the predicted noise level is 84%, or conversely, the risk that the actual noise level will be higher than the predicted noise level is 16%; and
- for a 90% and 95% confidence that the actual (or true) noise level will be less than the predicted noise level, the following engineering margins should respectively be added to the modelling results 5.0dB(A) and 6.4dB(A) .

Figures 2, 3 and 4 present the above uncertainties in terms of design level risks using a normal distribution risk profile with 50%, 84% and 95% confidence in compliance.

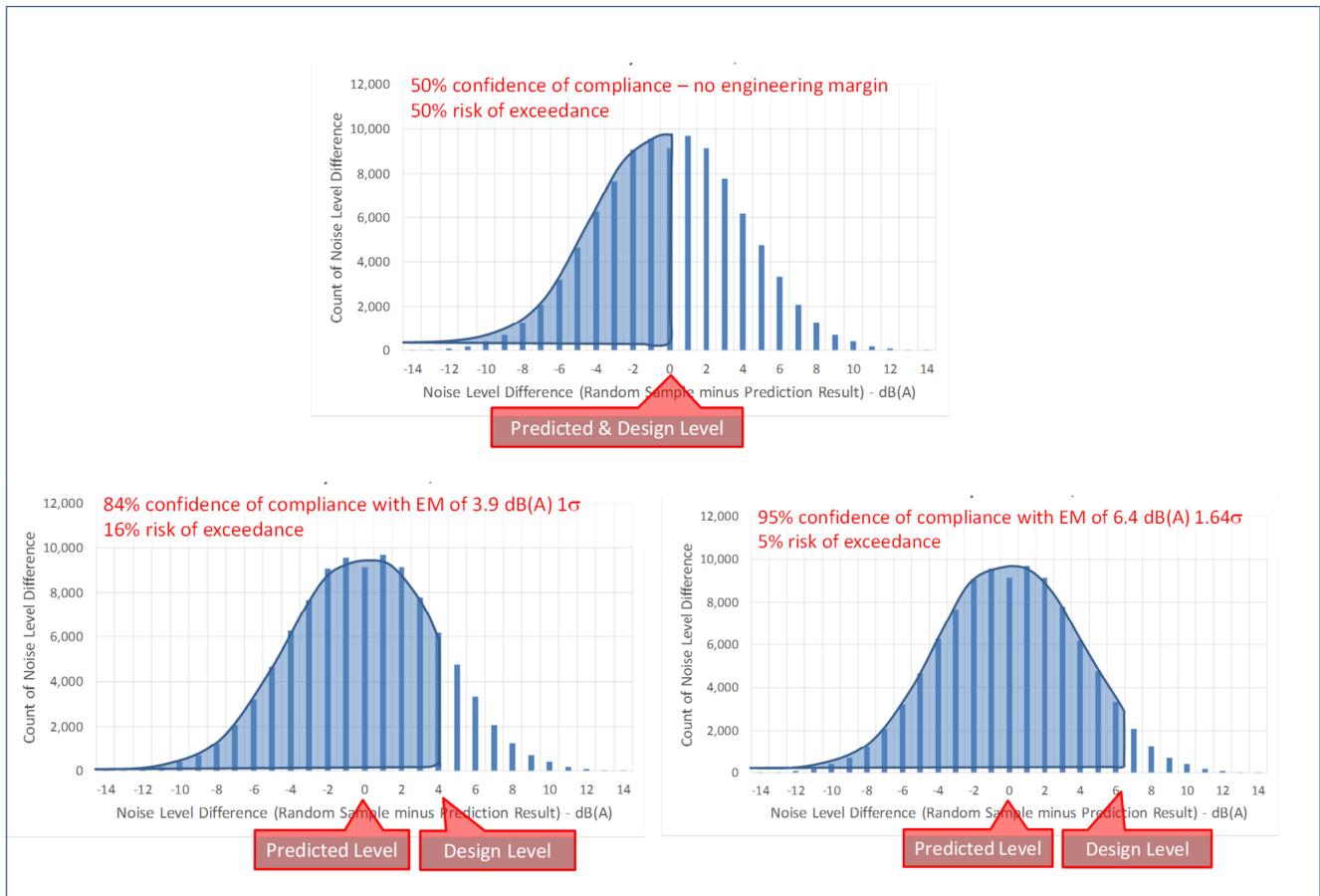


Figure 2, 3 & 4 – Design Level Risk with 50%, 84% & 95% Compliance Confidence

6. CONCLUSIONS AND RECOMMENDATIONS

On projects where there is limited or only high-level information relating to the source, path and receiver components, the uncertainty associated with GBNV predictions can be large. Based on some references [KTE Rail, 2016], prediction uncertainties of up to 10dB(A) have been reported and sometimes applied as a safety factor (engineering margin) on underground railway projects. During the detailed design stage of projects, large safety factors can be very costly in terms of the required mitigation measures.

Prediction uncertainties were determined based on the methodologies described in the International Standard ISO/IEC Guide 98-3 ‘Guide to the expression of uncertainty in measurement’ (GUM).

Field measurement data was utilised to reduce the uncertainty associated with key modelling input parameters (source, propagation path and receiver). For other input parameters, the uncertainty was established via published data and engineering judgement. The overall prediction uncertainty was then calculated based on guidance in the GUM and was independently validated using Monte Carlo simulation.

In summary, by undertaking field measurements and establishing uncertainties for all input modelling parameters, the overall confidence in noise and vibration predictions can be quantified using GUM. At the selected example location, the level of uncertainty was found to be significantly lower than originally estimated. This in turn can assist in reducing engineering design margins with subsequent project mitigation cost reduction benefits.

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